

Lecture 9: Flux and the flux integral

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1 Flux

In summary of the last few lectures, we have two line integrals that we're capable of taking right now. The first,

$$\int_C f(x, y, z) \, ds,$$

is the scalar line integral, which accumulates *the value of a scalar function f* along the curve C . The second,

$$\int_C \mathbf{F} \cdot d\mathbf{r} = \int_C M \, dx + N \, dy + P \, dz = \int_C \mathbf{F} \cdot \mathbf{T} \, ds,$$

is the vector line integral, which accumulates *the amount that the vector field \mathbf{F} follows C* along the curve C .

Both of these are equally valid in two or three dimensions; in fact, if we wanted to generalize everything we've done for these integrals to \mathbb{R}^n , nothing would change. Flux, the new quantity we want to introduce, is different: it will only correspond to a line integral when we're working in \mathbb{R}^2 .

The reason is that **flux** is a measure of how much a vector field \mathbf{F} crosses a boundary. Imagine stretching out a net in a body of water, or flying a kite: in both cases, you may well be interested in knowing how much water (or air) is crossing this boundary each second.

To draw a boundary between two parts of \mathbb{R}^n , you need an $(n - 1)$ -dimensional object. In \mathbb{R}^2 , you can separate two regions by drawing a curve. In \mathbb{R}^3 , however, it takes a surface to separate two regions. If you stretch your imagination, you might be able to picture \mathbb{R}^4 (4-dimensional space) and how it takes a 3-dimensional boundary there to separate two regions.

For this reason, we will only consider flux in \mathbb{R}^2 today, which we'll be able to describe as a line integral. We will return to flux when we begin working with surface integrals in \mathbb{R}^3 .

In two dimensions, the flux of \mathbf{F} across a curve C will measure *the amount that the vector field \mathbf{F} crosses C* . It is a signed quantity: \mathbf{F} can cross C in either direction, and we want these effects to have opposite signs.

For this reason, we need C to have an orientation, but the meaning we attach to the orientation is different. For the ordinary vector line integral, an orientation of C was a direction along C . For the flux line integral, an orientation of C is a direction *across* C . Which way of crossing C do we consider "positive", and which way do we consider "negative"?

¹This document comes from the Math 3204 course webpage: <http://facultyweb.kennesaw.edu/mlavrov/courses/3204-fall-2023.php>

We will adopt a convention for turning one of these orientations into the other. This convention is arbitrary: you cannot deduce from first principles which decision we make here. The rule is:

- Our old notion of orientation for curve C in \mathbb{R}^2 gives a preferred “positive” direction of travel along C . As you’re traveling along C in the positive direction, one side of the curve is on the left, and one side is on the right. Our convention is that **the positive direction of crossing C is from left to right**.
- Going the other way, suppose that you have a curve C for which we’ve picked a preferred “positive” direction of crossing C . Then we can choose a direction of travel along C so that the positive direction of crossing C is going from your left to your right. That direction of travel is going to be our positive direction along C .
- As a special case, suppose C is a simple closed curve—“simple” meaning that it does not cross itself. In this case, C is the boundary of a region R in the plane.

By default, we prefer to measure the *outward* flux across C : that is, we want the positive direction of crossing C to be the direction leaving the region R . This means that we want the orientation along C to be chosen so that R is on our left. Therefore our default orientation of the boundary of R is the curve that goes *counterclockwise* around R .

Some examples where the flux across a curve is clearly positive or negative are shown in Figure 1. Of course, it’s possible for a vector field to have a flux across a curve that’s positive at some points, and negative in others. In that case, these contributions will partially cancel out when we compute the net flux across the curve.

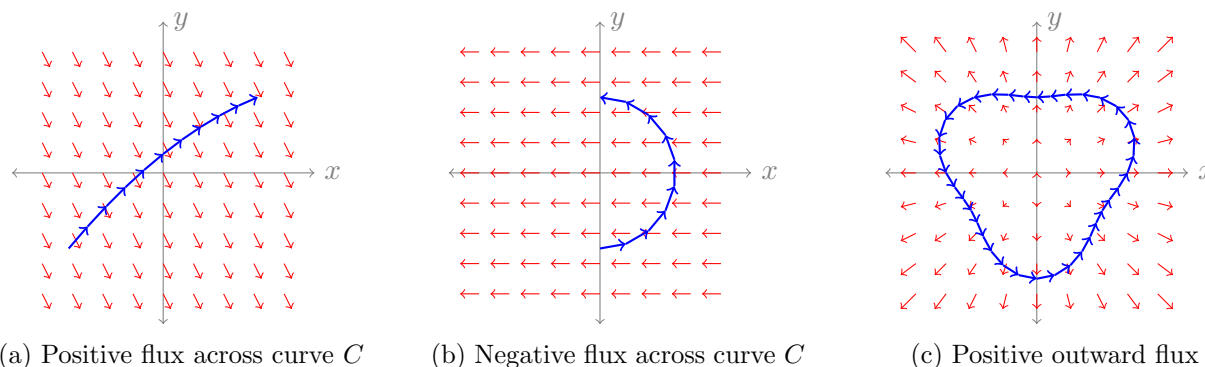


Figure 1: Three examples of positive and negative flux

2 Defining the flux integral

As motivation for the flux integral, consider the “scalar form” of the vector line integral:

$$\int_C \mathbf{F} \cdot \mathbf{T} \, ds.$$

Here, we think of the vector line integral (which, recall, computes the total amount that \mathbf{F} follows the curve C) in two steps. First, we compute $\mathbf{F} \cdot \mathbf{T}$ at each point on the curve C : this measures

how much \mathbf{F} follows the curve C at that point. Then, we integrate that quantity over the curve C . This works out by the identity

$$\int_{t=a}^b (\mathbf{F}(\mathbf{r}(t)) \cdot \mathbf{T}(t)) \left\| \frac{d\mathbf{r}}{dt} \right\| dt = \int_{t=a}^b \left(F(\mathbf{r}(t)) \cdot \frac{d\mathbf{r}/dt}{\|d\mathbf{r}/dt\|} \right) \left\| \frac{d\mathbf{r}}{dt} \right\| dt = \int_{t=a}^b \mathbf{F}(\mathbf{r}(t)) \cdot \frac{d\mathbf{r}}{dt} dt.$$

The flux integral will be defined starting from the same idea. We will write it as

$$\int_C \mathbf{F} \cdot \mathbf{n} ds$$

where \mathbf{n} will be a unit *normal vector* to the curve C , pointing in the positive direction crossing C . (As with \mathbf{T} , the vector \mathbf{n} is really a function $\mathbf{n}(t)$ that tells us the normal vector to the curve C at the point $\mathbf{r}(t)$.)

How do we compute \mathbf{n} , given \mathbf{T} ? The idea is that the positive direction *across* a curve, from our convention, is always a 90° clockwise turn from the positive direction *along* the curve.

We will denote this clockwise turn as $\mathbf{n} = \mathbf{T} \times \mathbf{k}$. Viewing \mathbf{n} and \mathbf{T} as three-dimensional vectors which happen to be parallel to the xy -plane, this \times is the cross product. If you haven't dealt with the cross product before (or in a while), we'll talk about it in detail later on in the semester. For now, we just need to know that it satisfies the rule

$$(a\mathbf{i} + b\mathbf{j}) \times \mathbf{k} = b\mathbf{i} - a\mathbf{j}.$$

You can check for yourself on a couple of examples that $b\mathbf{i} - a\mathbf{j}$ is really a 90° clockwise rotation of $a\mathbf{i} + b\mathbf{j}$. (Or you can look at the examples in Figure 2.)

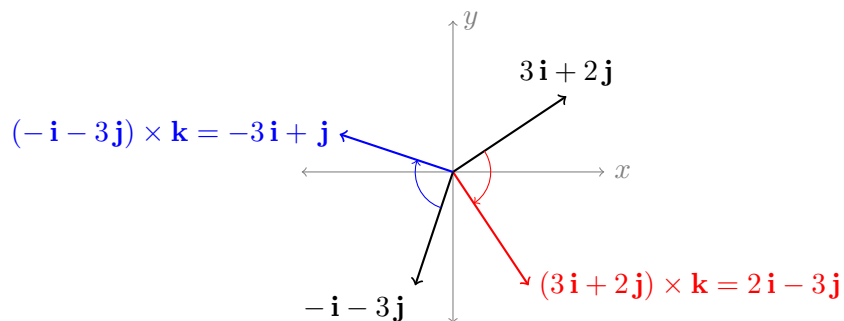


Figure 2: Rotating a vector with the $\times \mathbf{k}$ operation

Returning to our integral: the vector \mathbf{T} (really, $\mathbf{T}(t)$) is a scaled version of the vector $\frac{d\mathbf{r}}{dt}$, and the operations of rotating a vector and scaling a vector commute. So instead of rotating \mathbf{T} by 90° , we can rotate $\frac{d\mathbf{r}}{dt}$ by 90° . This gives us a formula for the flux integral:

$$\int_C \mathbf{F} \cdot \mathbf{n} ds = \int_{t=a}^b \mathbf{F}(\mathbf{r}(t)) \cdot \left(\frac{d\mathbf{r}}{dt} \times \mathbf{k} \right) dt.$$

Before we do an example, there is another way to look at the flux integral. If $\mathbf{r}(t) = (x(t), y(t))$, then $\frac{d\mathbf{r}}{dt} = \frac{dx}{dt} \mathbf{i} + \frac{dy}{dt} \mathbf{j}$, which means that $\frac{d\mathbf{r}}{dt} \times \mathbf{k} = \frac{dy}{dt} \mathbf{i} - \frac{dx}{dt} \mathbf{j}$. Now let's write \mathbf{F} as $M\mathbf{i} + N\mathbf{j}$ and expand out the integrand.

We get:

$$\begin{aligned}\mathbf{F}(\mathbf{r}(t)) \cdot \left(\frac{d\mathbf{r}}{dt} \times \mathbf{k} \right) &= (M(\mathbf{r}(t))\mathbf{i} + N(\mathbf{r}(t))\mathbf{j}) \cdot \left(\frac{dy}{dt}\mathbf{i} - \frac{dx}{dt}\mathbf{j} \right) \\ &= M(\mathbf{r}(t))\frac{dy}{dt} - N(\mathbf{r}(t))\frac{dx}{dt}.\end{aligned}$$

So it makes sense to write the flux integral as

$$\int_C \mathbf{F} \cdot \mathbf{n} \, ds = \int_{t=a}^b \left(M(\mathbf{r}(t))\frac{dy}{dt} - N(\mathbf{r}(t))\frac{dx}{dt} \right) dt = \int_C M \, dy - N \, dx,$$

in a similar way to how we can write the vector line integral as

$$\int_C \mathbf{F} \cdot d\mathbf{r} = \int_C M \, dx + N \, dy.$$

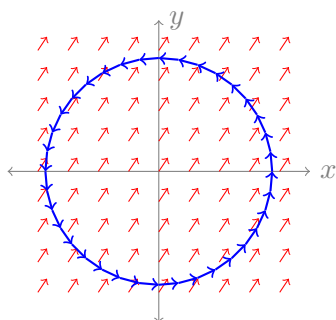
From this point of view, the integral of a differential 1-form like, say, $e^{x+y} dx + \cos y dy$ around C is indifferent to how we arrived at it. We can think of it as the integral of $\mathbf{F}_1 = e^{x+y}\mathbf{i} + \cos y\mathbf{j}$ along C , or we can think of it as the flux integral of $\mathbf{F}_2 = \cos y\mathbf{i} - e^{x+y}\mathbf{j}$ across C : either way, we would arrive at the integral

$$\int_C e^{x+y} dx + \cos y dy$$

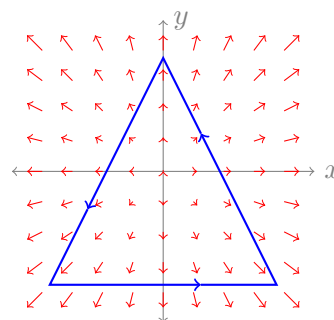
which we would compute in the same way.

3 Examples of flux integrals

First, let's do a quick example which we can expect to be 0. Take \mathbf{F} to be the constant vector field $2\mathbf{i} + 3\mathbf{j}$, and take C to be the counterclockwise unit circle. The flux of \mathbf{F} across C is the flux of \mathbf{F} *outward* from the unit circle... but we expect this to be 0, because on net, \mathbf{F} is neither entering nor leaving the unit circle. The amount that \mathbf{F} enters the circle from one side is exactly equal to the amount that \mathbf{F} leaves the circle from the other side. (See Figure 3a.)



(a) Outward flux of the vector field $\mathbf{F} = 2\mathbf{i} + 3\mathbf{j}$ across the unit circle



(b) Outward flux of the vector field $\mathbf{F} = x\mathbf{i} + y\mathbf{j}$ across the boundary of a triangle

Figure 3: Two flux integrals

We can verify that this intuition is correct by computing the flux integral.

If we parameterize the unit circle by $\mathbf{r}(t) = (\cos t, \sin t)$, then $\frac{d\mathbf{r}}{dt} = -\sin t \mathbf{i} + \cos t \mathbf{j}$, and therefore $\frac{d\mathbf{r}}{dt} \times \mathbf{k} = \cos t \mathbf{i} + \sin t \mathbf{j}$. In other words, $\frac{d\mathbf{r}}{dt} \times \mathbf{k}$ is equal to the radial vector pointing from the origin to $\mathbf{r}(t)$. This makes sense: the normal vector pointing out of the circle is the vector pointing directly away from $(0, 0)$, the center of the circle.

The vector field \mathbf{F} is $2\mathbf{i} + 3\mathbf{j}$, which we don't even need to evaluate at $\mathbf{r}(t)$, because it's constant. Therefore $\mathbf{F}(\mathbf{r}(t)) \cdot \left(\frac{d\mathbf{r}}{dt} \times \mathbf{k}\right)$ is equal to $2\cos t + 3\sin t$, and the flux integral is equal to

$$\int_{t=0}^{2\pi} (2\cos t + 3\sin t) dt = (2\sin t - 3\cos t) \Big|_{t=0}^{2\pi} = 0.$$

By the way, there's a trend you should grow used to seeing in these integrals: when you integrate $\sin t$ or $\cos t$ over an entire period of that function, you get 0.

Now let's do another integral. Here, our vector field will be the expanding vector field $\mathbf{F} = x\mathbf{i} + y\mathbf{j}$. Our curve will be the boundary of the triangle with corners at $(1, -1)$, $(0, 1)$, and $(-1, -1)$. We want the outward flux across this boundary, so the curve should be oriented counterclockwise.

The triangle has a piecewise boundary, so we'll compute the flux integral piece by piece, and we'll see three ideas as we go.

First, the piece from $(1, -1)$ to $(0, 1)$. This is parameterized by $\mathbf{r}(t) = (1-t, 2t-1)$, where $t \in [0, 1]$. This means that $\frac{d\mathbf{r}}{dt} = -\mathbf{i} + 2\mathbf{j}$, and $\frac{d\mathbf{r}}{dt} \times \mathbf{k} = 2\mathbf{i} + \mathbf{j}$. Meanwhile, $\mathbf{F}(\mathbf{r}(t)) = (1-t)\mathbf{i} + (2t-1)\mathbf{j}$, so the flux integral across this side of the triangle is

$$\int_{t=0}^1 ((1-t)\mathbf{i} + (2t-1)\mathbf{j}) \cdot (2\mathbf{i} + \mathbf{j}) dt = \int_{t=0}^1 (2 - 2t + 2t - 1) dt = \int_{t=0}^1 1 dt = 1.$$

Second, the piece from $(0, 1)$ to $(-1, -1)$. Here, we'll use the other expression for the flux integral: it is

$$\int_C M dy - N dx = \int_C x dy - y dx = \int_{t=0}^1 \left(x(t) \frac{dy}{dt} - y(t) \frac{dx}{dt} \right) dt.$$

The parameterization of this line segment is $\mathbf{r}(t) = (-t, 1-2t)$, where $t \in [0, 1]$. Therefore $x(t) = -t$, $y(t) = 1-2t$, $\frac{dx}{dt} = -1$, and $\frac{dy}{dt} = -2$, so we get

$$\int_{t=0}^1 (-t(-2) - (1-2t)(-1)) dt = \int_{t=0}^1 1 dt = 1.$$

It's not surprising that this is identical to the previous integral: these two sides of the triangle are symmetric.

For the final piece, from $(-1, -1)$ to $(1, -1)$, we'll think of the flux integral in its "scalar integral version": as

$$\int_C \mathbf{F} \cdot \mathbf{n} ds.$$

We can look at the boundary and directly see what \mathbf{n} should be: it is the unit normal vector pointing out of this boundary of the circle, and so it should point straight down: $\mathbf{n} = -\mathbf{j}$. (In general, \mathbf{n} is a function of t , but here it is a constant function.) Therefore $\mathbf{F} \cdot \mathbf{n} = (x\mathbf{i} + y\mathbf{j}) \cdot (-\mathbf{j}) = -y$.

Moreover, $-y$ is the constant 1 over this entire piece, and the scalar line integral of 1 over any curve is just its arc length. The length of this side of the triangle is 2, so the flux across it is 2. We get a total flux of $1 + 1 + 2 = 4$ out of the triangle.